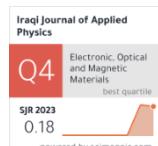


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# Optimization of Si/SiGe HBT Architecture Integrated in 28-nm FD-SOI BiCMOS Technology

This work aims to investigate a new Si/SiGe HBT in the fully depleted silicon on insulator technology (FD-SOI 28 nm). The epitaxial extrinsic base isolated from the collector (EXBIC) architecture has been used in this technology to reduce base resistance and enable cut-off frequencies to exceed 400 and 600 GHz for transition frequency  $f_t$  and maximum oscillation frequency  $f_{max}$ , respectively. Static and dynamic characteristics of the FD-SOI 28 nm have been evaluated using COMSOL multiphysics software. The technology achieved at base-emitter voltage of 0.83V, a value of 346 and 763.35 GHz for  $f_t$  and  $f_{max}$ , respectively. To further enhance frequency performance, architecture parameters such as germanium concentration, extrinsic base doping, emitter height and width are optimized achieving  $f_t$  of 360 GHz and  $f_{max}$  of 900 GHz. The results demonstrate the potential of using the SiGe HBTs based on the FD-SOI technology in the RF modules and THz systems.

**Keywords:** Silicon devices; SiGe structures; Bipolar transistors; BiCMOS technology; COMSOL  
Received: 7 July; Revised: 24 September; Accepted: 1 October 2025; Published: 1 January 2026

## 1. Introduction

The growing demands of customers in micro and nanotechnology industries, modern wireless communications systems accentuates the development of fundamental component capable of operating at higher frequencies [1,2]. Currently, electronic devices are fabricated with high cut-off frequencies exceeding 370 GHz, facilitating their applications in the millimeter-wave and THz bands [3,4].

BiCMOS technologies are particularly attractive for these type of applications due to their ability to combine high integration, high performance and low cost [5]. Among the various options, components based on heterojunction structures stand out as the most promising candidates for achieving the required functional frequencies while maintaining low noise levels [6]. The creation of Si/SiGe HBT technologies are known for their ability to reach performance frequencies in the terahertz range, offering significant potential for the development of ultra-fast electronic circuits. SiGe alloys are especially well-suited for these devices due to their narrower bandgap compared to pure silicon. Introducing SiGe alloys into the base of HBT's makes it feasible to modify the silicon energy bands [7-9].

The transistor architecture is a key factor in performance enhancement. One of the most widely adopted self-aligned architecture is the Double Polysilicon Self-Aligned (DPSA), which uses Selective Epitaxial Growth of the base (SEG). This architecture has been used and developed by STMicroelectronics in BiCMOS 55nm technology, achieving transition frequency  $f_t$  of 320 GHz and maximum oscillation

frequency  $f_{max}$  of 380 GHz [10,11]. However, the BiCMOS55 suffers from high extrinsic base resistance, which remains the primary limitation in achieving better performance compared to the transistor of IHP, which reaches for the same node a maximum frequency of 570 GHz. To overcome these limitations and to improve frequency performances, beyond 600 GHz and 400 GHz for maximum and transition frequency, a new technology of SiGe HBT integrated on fully depleted silicon on insulator FD-SOI, with an emitter width of 28 nm, has been developed. The FD-SOI 28 nm technology is manufactured based on Epitaxial eXtrinsic base isolated from the Collector (EXBIC) architecture, which is built on two important features: (i) an epitaxial boron in-situ-doped lateral base link reduces the extrinsic base resistance, (ii) an isolation (buried oxide layer BOX) implanted between the extrinsic base and the collector. The latter prevents boron diffusion and reduces the base collector capacitance; and also, offers the ability to control the collector profile using an intrinsic in-situ doped collector [12,13].

The main purpose of adding the buried oxide (BOX) is to provide a solution with high performance and low power consumption. This is achieved by electrically isolating the extrinsic base from the collector via the BOX layer, which significantly decreases the base-collector capacitance  $C_{BC}$ . As demonstrated in [12], increasing the BOX layer thickness leads to a significant decrease in  $C_{BC}$ , resulting in a marked improvement in both transition frequency  $f_t$  and maximum frequency  $f_{max}$ .

Compared to silicon bulk, the SOI technology frequently offers 20 to 30 % better performance at the same operating voltage. These advantages make the technology based on SOI layer particularly attractive for high performance applications including wireless communication, radar and THz systems [14].

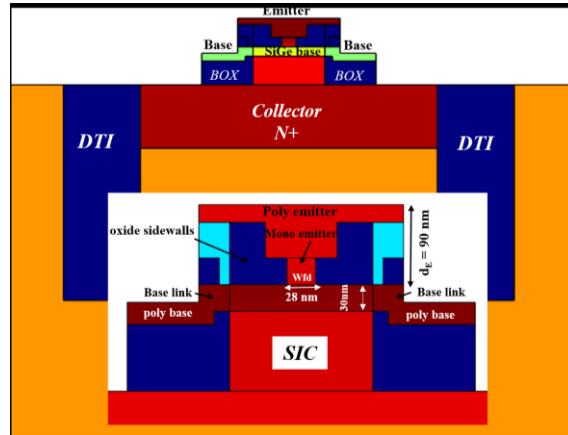
In order to further enhance the electrical performance of FD-SOI 28 nm technology, particularly the frequency  $f_t$  and  $f_{max}$ , an optimization of electrical parameters is the main purpose of this work. The first part of this paper describes the architecture used in the FD-SOI 28 nm technology and its electrical performance. The simulation results enable a review of static and dynamic characteristics, including base and collector currents ( $I_C$ ,  $I_B$ ), static gain ( $\beta$ ), transition and maximum oscillation frequency ( $f_t$  and  $f_{max}$ ). Furthermore, a comparison of the frequency performance between the studied technology and the BiCMOS55 was performed to better evaluate the impact of the EXBIC architecture. To validate our results, a comparative analysis was also conducted against results reported in the literature. The second part focuses on optimizing several electrical and geometrical parameters, such as germanium concentration  $x$ , extrinsic base doping  $N_{ab}$ , emitter height  $d_E$  and emitter width  $w_{fd}$ , to further enhance the cut-off frequency  $f_t$  and  $f_{max}$  before initiating the process trials.

This paper demonstrates significant potential for THz operation, confirming the suitability of the FD-SOI technology for advanced RF front-end integration. This study also provides valuable insights into the co-design of device geometry and technology parameters for next-generation SiGe HBTs in sub-THz applications.

## 2. Physical Design and Numerical Simulation

The investigated structure consists of NPN SiGe HBT integrated into the FD-SOI 28nm technology with a frequency performance of  $f/f_{max} = 380/780$  GHz [15]. The device structure shown in Fig. (1) consists of a heavily-doped collector  $n^{++}$  ( $3 \times 10^{19} \text{ cm}^{-3}$ ), sandwiched between two shallow trench isolations STI, and an intrinsic collector (n) formed by selective epitaxial growth of arsenic doped silicon SIC with a doping of  $7 \times 10^{16} \text{ cm}^{-3}$ . The base region is composed of a thin intrinsic SiGe base (30 nm) with a germanium concentration of 20% and a doping of  $5 \times 10^{18} \text{ cm}^{-3}$  [16]. This layer is aligned with an extrinsic base composed of a polysilicium base and base link, which is more heavily doped ( $4 \times 10^{19} \text{ cm}^{-3}$ ). The emitter section is composed of two parts, a thin mono-silicon layer and relatively thicker polysilicon layer. The total height of the emitter is 90 nm and a Gaussian doping profile ranging from  $2 \times 10^{21} \text{ cm}^{-3}$  to  $9 \times 10^{16} \text{ cm}^{-3}$  (Fig. 2) [17]. The BOX layer in this structure is used to separate the extrinsic base to the extrinsic collector. In addition, oxide sidewalls are

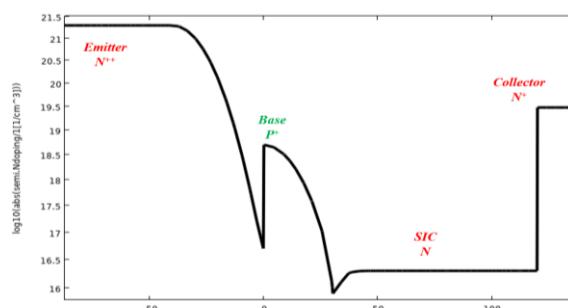
used between the selective implanted collector SiC and the extrinsic base, which avoid boron diffusion from the intrinsic base to the collector. As a result, reducing base-collector capacitance and extrinsic base resistance [13]. Table (1) summarized the main electrical parameters of the studied architecture.



**Fig. (1) The final structure of the EXBIC structure used in the 28nm FD-SOI technology under COMSOL software**

**Table (1) Electrical parameters of the SiGe HBT integrated in FD-SOI BiCMOS 28nm**

Region	Emitter	Poly base	SiGe base	SiC	Collector
Height (nm)	90	45	30	90	200
Doping (cm <sup>-3</sup> )	$2 \times 10^{21}$	$4 \times 10^{19}$	$5 \times 10^{18}$	$5 \times 10^{16}$	$3 \times 10^{19}$



**Fig. (2) Vertical doping profile of the FD-SOI 28nm under COMSOL.**

## 2.1. Simulation Models

In our study, the semiconductor Module of the COMSOL software, which is designed for simulating and analyzing semiconductor devices, has been used to simulate the electrical properties of the studied HBT. It provides a set of physics interfaces and features that enable detailed modeling of electrical, thermal, and quantum effects in semiconductor structures.

### 2.1.1. DDM model

**2.1.1. DDM model**  
The drift diffusion model DDM is a fundamental approach used to simulate charge transport in semiconductor devices. It combines the movement of

electrons and holes caused by electric fields (drift) and concentration differences (diffusion), along with electrostatic effects described by Poisson's equation. This model couples Poisson's equation with the continuity equations for carriers, including generation and recombination effects.

Poisson's equation:

$$\nabla \cdot (-\epsilon_r * \nabla \cdot \nabla) = q(P - N + N_D^+ + N_A^-) \quad (1)$$

Electrons and holes continuity equations:

$$\frac{\partial N}{\partial t} = +\frac{1}{q}(\nabla \times J_n) - U_n \quad (2)$$

$$\frac{\partial P}{\partial t} = -\frac{1}{q}(\nabla \times J_p) - U_p \quad (3)$$

where N and P are the concentration of electron and hole,  $N_D^+$  and  $N_A^-$  are the concentration of ionization of impurities and  $\epsilon_r$  is the relative permittivity of the material

The rate net of electronic and hole recombination  $U_n$  and  $U_p$  are represented in equations (4) and (5), where  $R_n$  and  $R_p$  are the recombination rates for electrons and holes and,  $G_n$  and  $G_p$  are the generation rates of electrons and holes [18].

$$U_n = R_n - G_n \quad (4)$$

$$U_p = R_p - G_p \quad (5)$$

Equations (6) and (7) are derived from Maxwell:

$$J_n = +qN\mu_n \frac{d\phi_n}{dx} \quad (6)$$

$$J_p = -qP\mu_p \frac{d\phi_p}{dx} \quad (7)$$

The current densities  $J_n$  and  $J_p$  are depend of mobility of electron and hole  $\mu_p$  and  $\mu_n$ , and also the quasi-fermi potentials of the carriers  $\phi_n$  and  $\phi_p$  [19].

### 2.1.2. Mobility model

The Arora mobility model is the most widely used in COMSOL Multiphysics for semiconductor device simulation, as it accounts for both phonon scattering and ionized impurity scattering, unlike simpler models such as the power law model, which only consider phonon scattering. Arora model directly computes mobility from parameters such as doping and temperature without requiring additional external inputs, which makes it autonomous as a basis for mobility. This model thus offers a better accuracy for doped semiconductors, providing a more realistic estimate for heavily doped regions than a phonon-only model [20]. The general equation of this model are:

$$\mu_{n,ar} = \mu_{n,min} + \frac{\mu_{n,0}}{1 + \left(\frac{N}{N_{n,0}}\right)\left(\frac{N}{N_{n,0}}\right)^{\alpha_n}} \quad (8)$$

$$\mu_{p,ar} = \mu_{p,min} + \frac{\mu_{p,0}}{1 + \left(\frac{N}{N_{p,0}}\right)^{\alpha_p}} \quad (9)$$

with

$$N = N_a^- + N_d^+ \quad (10)$$

$$\mu_{n,min} = \mu_{n,min}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_1} \quad (11)$$

$$\mu_{p,min} = \mu_{p,min}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_1} \quad (12)$$

$$\mu_{n,0} = \mu_{n,0}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_2}, \mu_{p,0} = \mu_{p,0}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_2} \quad (13)$$

$$N_{n,0} = N_{n,0}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_3}, N_{p,0} = N_{p,0}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_3} \quad (14)$$

$$\alpha_{n,0} = \alpha_{n,0}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_4}, \alpha_{p,0} = \alpha_{p,0}^{\text{ref}} \left(\frac{T_1}{T_{\text{ref}}}\right)^{\beta_4} \quad (15)$$

The various variables mentioned in the above system of equations:  $\mu_{n,ar}$ ,  $\mu_{p,ar}$  are Arora mobility of electron and hole.  $\mu_{n,min}$ ,  $\mu_{p,min}$  minimum mobility of electron and hole.  $\mu_{n,0}$ ,  $\mu_{p,0}$  initial mobility,  $\mu_{n,0}^{\text{ref}}$ ,  $\mu_{p,0}^{\text{ref}}$  are the reference mobility. N,  $N_{n,0}$ ,  $N_{p,0}$ ,  $N_{n,0}^{\text{ref}}$ ,  $N_{p,0}^{\text{ref}}$  are concentration of dopants, electron impurities, hole impurities, electron and hole reference concentrations successively.  $T_1$ ,  $T_{\text{ref}}$  are the ambient and reference temperature.  $\beta_1$ ,  $\beta_2$ ,  $\beta_3$ ,  $\beta_4$  are the exponent of minimum reference mobility, reference mobility and reference impurity concentrations of coefficient  $\alpha$ .

## 3. Electric Characteristics

### 3.1. Static Characteristics

Figure (3) shows gummel plots and static gain as a function of base-emitter voltage  $V_{BE}$ , varying from 0 to 1.1 V, while the base-collector voltage  $V_{BC}$  is fixed at 1.5 V. These graphs allow for a rapid evaluation of the ideality of the transistor currents, as indicated by the differences between the various curves. They also emphasize quasi-saturation effects, which are caused by high series resistance values [16]. At low injection regime ( $V_{BE} < 0.4V$ ), the base current  $I_B$  is influenced by recombination phenomena at the space charge zone. Consequently, only a small number of electrons reach the base, resulting in fewer charges in the collector. This is revealed on the curve by a very low base and collector currents, as well as a correspondingly low current gain. In the normal operating regime ( $0.4V < V_{BE} < 0.8V$ ), electron injection becomes sufficient to cross the base and reach the collector, the transistor exhibits amplifying behavior and the gap between the collector and base currents curves represents the static current gain. The linear variation of the currents with  $V_{BE}$  allows for the extraction of saturation currents and the ideality factors of the junctions, for  $V_{BE} = 0.55$  V the transistor achieves its maximum static gain of  $\beta_{\text{max}} = 3742$ . At high carrier injection ( $V_{BE} > 0.8V$ ), the current gain is significantly reduced due to the Kirk effect, which corresponds to a change in the electric field at the collector junction. The collector current density rises above the collector doping concentration due to the increased electron injection from the emitter into the base. This condition causes a reduction in the electric field in the space charge region between base and collector, which normally prevents hole diffusion out of the base. As the field decreases, the hole profile extends toward the

collector, forming a quasi-neutral region and leading to a virtual increase of the base thickness. This base enlargement results in a significant degradation in current gain [21].

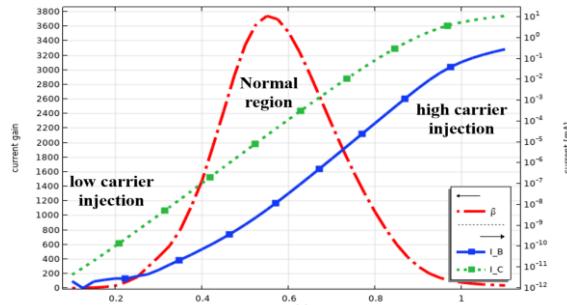


Fig. (3) Variation of  $I_B$ ,  $I_C$  and  $\beta$  as a function of  $V_{BE}$  of the FD-SOI28nm

Figure (4) presents the output characteristics  $I_C$  ( $V_{CE}$ ) with different values of base current  $I_B$  ( $1\mu A$ ,  $2\mu A$ ,  $3\mu A$ ). It can be noticed that in the normal regime ( $V_{CE} < 0.3V$ ), the collector current increases progressively with  $V_{CE}$  due to the purely resistive behavior of the transistor's. However, when the voltage increases ( $0.3V < V_{CE} < 3V$ ), the current  $I_C$  is minimally depended to  $V_{CE}$ , indicating current saturation (saturation zone). At height value of collector-emitter voltage ( $V_{CE} > 3V$ ), the current  $I_C$  increases slightly instead of stabilizing indicating the beginning of the Kirk effect.

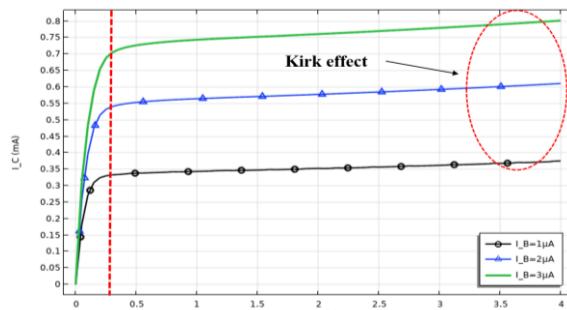


Fig. (4) Variation of collector current  $I_C$  as a function of  $V_{CE}$  for different base current  $I_B$

### 3.2. Dynamic Characteristics

Due to the application of HBTs in the THz domains, our focus is on their dynamic performances, specifically the transition frequency  $f_t$  and maximum oscillation frequency  $f_{max}$ . These frequencies are described by the following equations:

$$f_t = \frac{1}{2\pi(\tau_f + \frac{KT}{qI_C}(C_{BC} + C_{BE}) + (R_C + R_E)C_{BC})} \quad (16)$$

$$f_{max} = \frac{f_t}{\sqrt{(8\pi R_B C_{BC})}} \quad (17)$$

The transition frequency  $f_t$  depends on various parameters including base-collector capacitance, emitter-base capacitance, transit time and resistances of the collector, emitter and base:  $C_{BC}$ ,  $C_{BE}$ ,  $\tau_f$ ,  $R_C$ ,  $R_E$  and  $R_B$ , respectively. Whereas,  $f_{max}$  varies inversely

with the base-collector capacitance  $C_{BC}$  and base resistor  $R_B$ , which in turn is inversely proportional to the base doping  $N_{ab}$  [22].

The 28-nm FD-SOI technology is considered a promising solution to overcome the limitations of the DPSA-SEG architecture employed in BiCMOS55 technology and also to improve frequency performance. This part presents a comparison of frequency  $f_t$  and  $f_{max}$  of both technologies, COMSOL simulations results are presented in Fig. (5). The moving from BiCMOS55 to FD-SOI 28 nm leads to an increase in frequency performance specifically the maximum frequency  $f_{max}$ , confirming the effectiveness of the EXBIC architecture in reducing base resistance and capacitance.

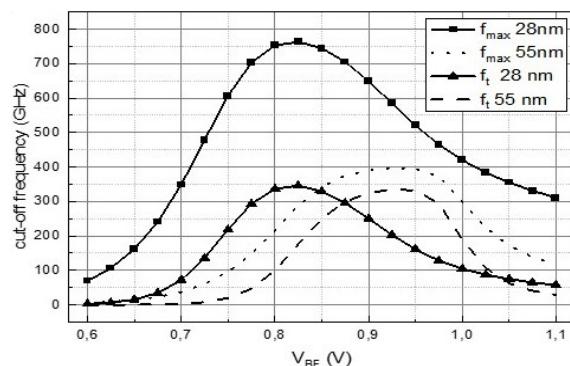


Fig. (5) Variation of  $f_t$  and  $f_{max}$  as a function of  $V_{BE}$  for both technologies FD-SOI 28nm and BiCMOS55 simulated using COMSOL software [23]

To validate our results, a comparative analysis was carried out using TCAD simulation data and experimental results available in the literature (Fig. 6). Table (2) summarizes the outcomes, the 28-nm FD-SOI technology achieves, at base-emitter voltage of  $0.83V$ , a value of  $346$  GHz and  $763.35$  GHz for  $f_t$  and  $f_{max}$ , respectively. These values are comparable to those obtained by Vu et al. [12], which indicates  $f_t/f_{max}=380/780$  GHz. In comparison, a value of  $f_t/f_{max}=334/397$  GHz has been obtained for BiCMOS55 using COMSOL software [23], which are close similar to TCAD simulation results reported in [11], which indicate  $f_t/f_{max}=320/380$  GHz. The minor deviations observed between our results and previously published work can be attributed to several modeling assumptions, such as idealized doping profile and simplified interface characteristics. The idealized doping profile corresponds to the use of an abrupt and uniform doping concentration (box profile type) in base and emitter region of the HBT, without accounting for diffusion effects. The simplified interface characteristics indicate that phenomena such as interface traps and surface roughness are neglected in our simulation. Furthermore, parasitic effects such as layout-induced capacitance and packaging-related effects were not explicitly taken into account in this study.

Table (2) Comparison between  $f_t$  and  $f_{max}$  of both technologies FD-SOI28 and BiCMOS55

Technology	$f_t$ (GHz)	$f_{max}$ (GHz)	Reference
28-nm FD-SOI	346	763.35	This work
28-nm FD-SOI	380	780	[27]
BiCMOS55	320	380	[11]
BiCMOS55	334	397	[23]

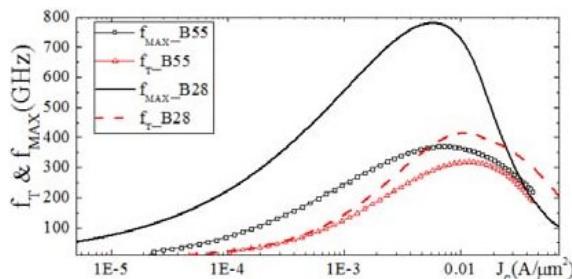


Fig. (6) Variation of  $f_t$  and  $f_{max}$  with the variation of collector current density for FD-SOI 28 nm and BiCMOS55 technologies using TCAD simulation by STMicroelectronics[27]

#### 4. Optimization of Technological Parameters of FD-SOI 28nm Technology

##### 4.1. Effect of Germanium Concentration

To investigate the influence of germanium content  $x$  in the  $\text{Si}_{1-x}\text{Ge}_x$  alloy on transistor operation and frequency performance, simulations were performed for various germanium concentrations (10%, 20%, and 30%). As shown in figures (7) and (8), both the base and collector currents increase proportionally with increasing germanium concentration, leading to a significant enhancement in the static current gain  $\beta$ , which reaches a peak value of 3855 at  $x=30\%$  (Table 3). This increase in current is primarily attributed to a reduction in the potential barrier encountered by electrons moving from the emitter to the base, which explains the increase in electron injection efficiency [24]. However, a decrease in  $f_t$  is observed, gradually from 352.2 to 337.8 GHz as the germanium concentration increases from 10% to 30% (Fig. 9). This degradation is mainly attributed to an increase in base transit time  $\tau_B$  caused by the reduction in electron mobility due to increased alloy scattering within the base [25].

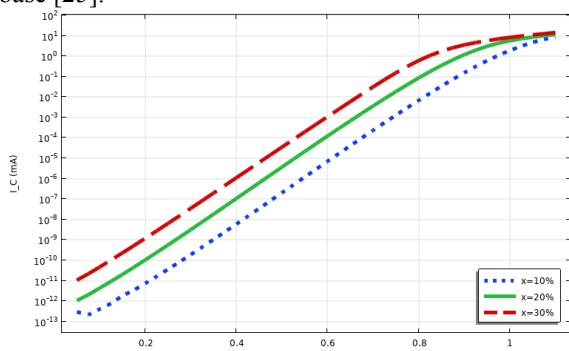


Fig. (7) Variation of  $I_C$  as a function of  $V_{BE}$  for different germanium concentration

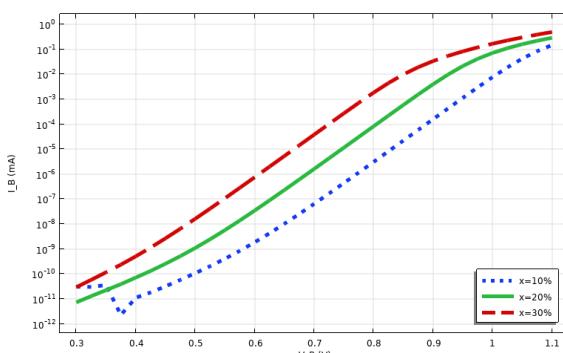


Fig. (8) Variation of  $I_B$  as a function of  $V_{BE}$  for different germanium concentration

Table (3) Static and dynamic performance for different germanium concentration  $x$

$x$	$I_C$ (mA)	$I_B$ (mA)	$\beta$	$f_t$ (GHz)	$f_{max}$ (GHz)
10 %	$1.18 \times 10^{-6}$	$3.2 \times 10^{-10}$	3689	352.2	771.3
20 %	$2.19 \times 10^{-5}$	$5.85 \times 10^{-9}$	3742	345.9	763.35
30 %	$2.999 \times 10^{-4}$	$7.79 \times 10^{-8}$	3855	337.8	754.3

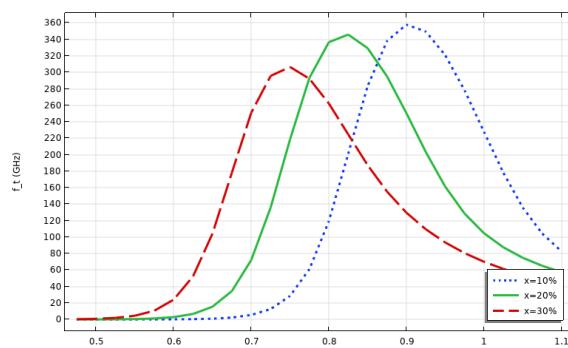


Fig. (9) Variation of  $f_t$  as a function of  $V_{BE}$  for different germanium concentration

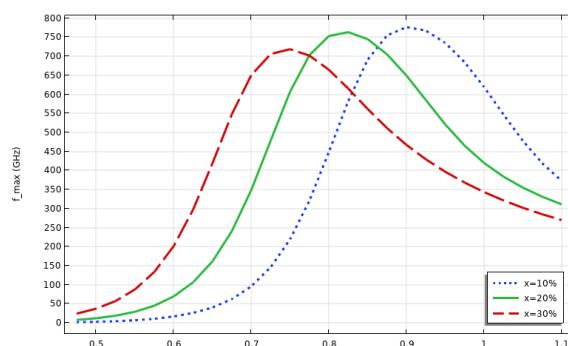


Fig. (10) Variation of  $f_{max}$  as a function of  $V_{BE}$  for different germanium concentration  $x$

These results are in good agreement with those reported by Derrickson et al. [26], where the peak value of  $f_t$  is achieved at lower germanium concentration. The frequency  $f_{max}$  decreases with the decrease of  $f_t$ , dropping from 771.3 to 754.3 GHz (Fig. 10). The electron and hole mobility increase at high Ge concentration (>85%) explaining that as the germanium concentration increase the SiGe alloy becomes as Ge-type and its physical properties

become closer to those of germanium than silicon [25].

#### 4.2. Effect of Extrinsic Base Doping

This section investigates the effect of increasing extrinsic base doping  $N_{ab}$  on the electrical properties of the 28nm FD-SOI. The primary goal of this approach is to enhance the maximum oscillation frequency  $f_{max}$  by reducing the base resistance  $R_B$ , which made up of extrinsic base resistance  $R_{Ex}$  and intrinsic base resistance  $R_{SiGe}$ , as shown in the following equations:

$$R_B = R_{Ex} + R_{SiGe} \quad (18)$$

$$R_{Ex} = \frac{1}{qN_{ab}\mu_{ppoly}} \cdot \frac{2L_{Bpoly}}{d_{Bpoly}L_{HBT}} + \frac{1}{qN_{ab}\mu_{ppoly}} \cdot \frac{2L_{Blink}}{d_{Blink}L_{HBT}} \quad (19)$$

$$R_{SiGe} = \frac{1}{qN_{BSiGe}\mu_{pSiGe}} \cdot \frac{L_{BSiGe}}{d_{BSiGe}L_{HBT}} \quad (20)$$

$N_{BSiGe}$ ,  $N_{ab}$  are the intrinsic and extrinsic base doping.  $\mu_{ppoly}$ ,  $\mu_{pSiGe}$  are their hole mobility.  $L_{BSiGe}$ ,  $L_{Bpoly}$ ,  $L_{Blink}$  are base width of intrinsic, poly base and base link, respectively.  $d_{BSiGe}$ ,  $d_{Bpoly}$ ,  $d_{Blink}$  are their base depth and  $L_{HBT}$  is the length of the HBT. The coefficient 2 corresponds to the two extrinsic bases used in the EXBIC architecture (see Fig. 1).

Table (4) shows static and dynamic characteristics as a function of  $N_{ab}$ . As the doping increases from  $4 \times 10^{19}$  to  $9 \times 10^{20} \text{ cm}^{-3}$ , the space charge region becomes narrower, which increases carrier recombination within the base, leading to an increase in  $I_B$  while a slight decrease in  $I_C$  is obtained [26]. The observed current variations result in a slight decrease in  $\beta$  from 3742 for a concentration of  $4 \times 10^{20} \text{ cm}^{-3}$  to 3697 for a concentration of  $9 \times 10^{20} \text{ cm}^{-3}$ .

Table (4) Electric characteristics for different extrinsic base doping  $N_{ab}$

$N_{ab} (\text{cm}^{-3})$	$4 \times 10^{19}$	$8 \times 10^{19}$	$5 \times 10^{20}$	$7 \times 10^{20}$	$9 \times 10^{20}$
$R_E (\Omega)$	0.851	0.851	0.851	0.852	0.852
$R_B (\Omega)$	217.17	188.17	163.8	162.48	161.74
$C_{BC} (\text{fF})$	0.109	0.109	0.109	0.109	0.109
$C_{BE} (\text{fF})$	0.1589	0.1589	0.1589	0.159	0.159
$\beta$	3742	3734	3721.7	3714	3697
$f_t (\text{GHz})$	345.96	345.9	345.8	345.76	345.75
$f_{max} (\text{GHz})$	763.35	820	878.72	882.27	884.26

The frequency  $f_t$  is not noticeably changed with the increased doping due to the minor reduction in the internal width of the transistor (Fig. 11). A notable decrease in  $R_B$  is observed, due to a decrease in both the poly silicon base and base link resistances.  $C_{BC}$  remains unchanged. Consequently,  $f_{max}$  increases to 884.26 GHz for a doping of  $9 \times 10^{20} \text{ cm}^{-3}$  (Fig. 12). Our results confirm the findings of [27], where  $f_{max}$  reached a value of 835 GHz for a concentration of  $8 \times 10^{20} \text{ cm}^{-3}$ .

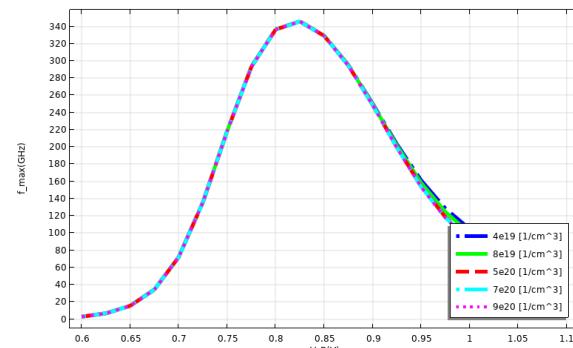


Fig. (11) Variation of the transition frequency  $f_t$  as a function of extrinsic base doping  $N_{ab}$

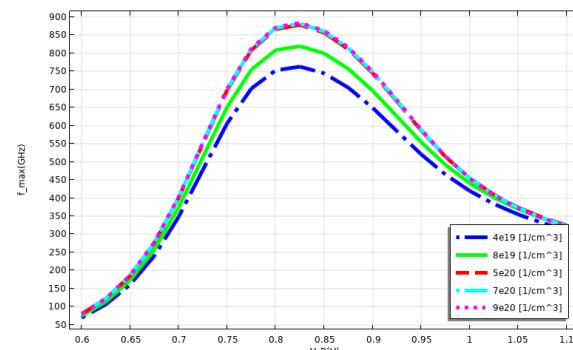


Fig. (12) Variation of the maximum frequency  $f_{max}$  as a function of extrinsic base doping  $N_{ab}$

#### 4.3. Effect of Emitter Height

In this section, we examine the impact of emitter height  $d_E$  on the electric characteristics of the FD-SOI 28 nm, using a germanium content of 20 % and fixed extrinsic base doping of  $9 \times 10^{20} \text{ cm}^{-3}$ . As shown in table (5), reducing  $d_E$  by 20% results in a decrease in  $\beta$  from 3697 to 2817, due to a slight increase in  $I_B$  by the recombination processes at the emitter [28].

Table (5) Static and dynamic characteristics for different emitter height  $d_E$

Emitter height (nm)	$d_E$	0.95 $d_E$	0.9 $d_E$	0.8 $d_E$
$R_E (\Omega)$	0.851	0.893	0.942	1.071
$R_B (\Omega)$	161.74	161.74	161.74	161.74
$C_{BC} (\text{fF})$	0.109	0.109	0.109	0.109
$C_{BE} (\text{fF})$	0.1589	0.1542	0.1495	0.1399
$\beta$	3697	3687	3583	2817
$f_t (\text{GHz})$	345.95	354	359	360
$f_{max} (\text{GHz})$	884.26	897.45	903.6	906

Furthermore, a slight increase in  $f_t$  from 345.75 to 360 GHz is observed (Fig. 13). This enhancement is due to a decrease in base-emitter capacitance  $C_{BE}$  accompanied by a significant reduction in emitter transit time  $\tau_E$ , which in turn decreases the total transit time  $\tau_f$  (Eq. 21 and 22). The decrease in  $\tau_E$  is due to a decrease in the distance that carriers crossed from the emitter to the base. The slight increase of  $R_E$  ( $\approx 0.20 \Omega$ ) is considered negligible relative to the more substantial change of  $\tau_E$ .  $R_B$  and  $C_{BC}$  remain

unchanged. As a result, the increase in  $f_t$  contributes to an improvement in  $f_{max}$  from 884 GHz to 900 GHz (Fig. 14).

$$\tau_E = \frac{(3d_E)^2}{2\beta D_{pE}} \quad (21)$$

$$\tau_f = \tau_E + \tau_{BC} + \tau_B \quad (22)$$

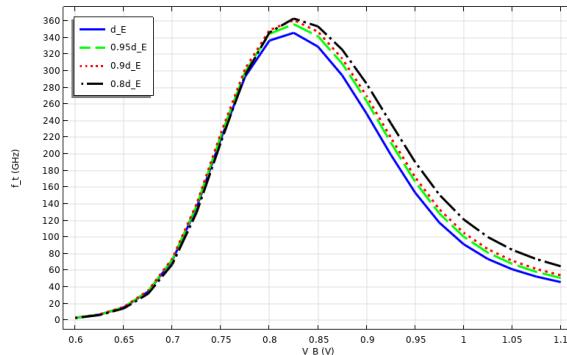


Fig. (13) Variation of the frequency  $f_t$  as a function of  $V_{BE}$  for different emitter height  $d_E$

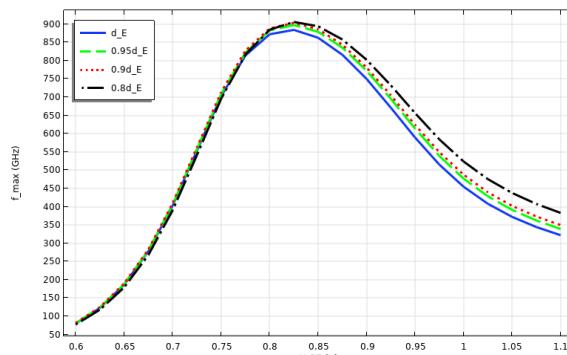


Fig. (14) Variation of the frequency  $f_{max}$  as a function of  $V_{BE}$  for different emitter height  $d_E$

#### 4.4. Effect of Emitter Width

Table (6) presents the electrical characteristics as a function of emitter width  $w_{fd}$ , using a germanium percentage of 20% and a base doping of  $4 \times 10^{19} \text{ cm}^{-3}$ . The results show that decreasing the emitter width leads to a slight reduction in both  $\beta$  and  $f_t$ . The latter results from a small reduction in the collector current  $I_C$  and the base-emitter capacitances  $C_{BE}$ , accompanied with a significant rise in the emitter resistance  $R_E$ . However,  $f_{max}$  improves as a result of the decrease in base resistance  $R_B$ , reaching a value of 903.5 GHz when the emitter width is reduced by 20 %. These results are in accordance with those reported in [27], which mentioned that reducing emitter width leads to a decrease in current gain and transition frequency, while the maximum frequency is enhanced as the width is reduced.

#### 5. Conclusion

The work discussed in this article focuses specifically on the electrical characteristics of a SiGe HBT integrated in FD-SOI 28 nm technology, using EXBIC architecture. This architecture offers two key

features: oxide sidewalls isolate the extrinsic base from the collector and reduce  $C_{BC}$ , while the epitaxial boron in-situ-doped lateral base link reduces  $R_B$ . Electrical performance simulation of the FD-SOI 28nm showed values of 346 and 760 GHz for  $f_t$  and  $f_{max}$ , respectively. To enhance both  $f_t$  and  $f_{max}$ , a combination of high extrinsic base doping  $N_{ab}$  and a reduction in emitter height  $d_E$  is necessary. A large emitter width  $w_{fd}$  increases significantly  $R_B$  leading to reduce  $f_{max}$  while  $f_t$  benefits from this expansion. Optimal values of the above mentioned increased significantly the value of  $f_t$  and  $f_{max}$  to 360 GHz and 0.9 THz, respectively. This improvement in the frequency performance may lead to a better implementation of such HBT technologies in terahertz applications.

Table (6) Transistor electric performances for different emitter width  $w_{fd}$

Emitter width (nm)	$w_{fd}$	0.95 $w_{fd}$	0.9 $w_{fd}$	0.8 $w_{fd}$
$R_B (\Omega)$	217.17	213.81	211.02	206.21
$R_E (\Omega)$	0.852	0.868	0.872	0.873
$C_{BC} (\text{fF})$	0.109	0.109	0.109	0.109
$C_{BE} (\text{fF})$	0.1589	0.1587	0.1585	0.1581
$\beta$	3697	3681	3618	3556
$f_t (\text{GHz})$	345.96	341.2	340	336.5
$f_{max} (\text{GHz})$	884.26	887.85	894.5	903.5

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